Comparison of Absolute Distance Measurement by Different Types of Dual Mode-Locked Fiber Lasers

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I. Introduction
Precise absolute distance measurement is very crucial for large-scale manufacturing. Classic multi-wavelength interferometry can be slow and subject to cyclic errors. In 2009, Coddington et al. had demonstrated the precise ranging with precision of ~200 nm by utilizing dual fully frequency stabilized 100 MHz fiber laser comb [1]. Dual-comb techniques, a subclass of the cross-correlation techniques, are particularly attractive because they can scan an entire range window quickly allowing for rapid update rates against multiple targets, and requiring no balancing of interferometer paths. Later, a simple linear cavity without any group velocity dispersion (GVD) compensation, dual 200 MHz free running mode-locked fiber lasers are demonstrated [2]. The dual laser are utilized for the ranging and the precision is also ~200 nm in averaging time of ~ 20 ms. Recently, a dual-comb nonlinear asynchronous optical sampling technique was demonstrated for the absolute distance measurement [3]. The pulse intensity was acquired directly from the time of flight measurement, and the data processing time was reduced without using Hilbert transform. However, the high power laser is required for the nonlinear frequency doubling effect. The repetition rate is stabilized to 250 MHz. It was also used for the ranging, and the precision was similar as the former cases. These three papers were with long pulse repetition rate, the ambiguity was smaller than 1 m.

In this paper, we utilized longer linear laser cavity with lower repetition rate of 70 MHz to obtain the larger non-ambiguity range of 2.1 m by asynchronous sampling technique. It is housing in a compact box for the long range industrial applications. The results are compared with a well GVD compensated ring cavity with a similar repetition rate of 100 MHz.

II. Experimental Setup

A. Laser Design

A1. Linear cavity mode-locked laser without any dispersion compensation

The experimental set up is depicted in Fig. 1. The laser employed here is an Erbium all fiber design operating at repetition rates of ~70 MHz, which corresponds to the time of flight non-ambiguity range of 2.1 m. The cavity design is a semiconductor saturable absorber mirror (SAM) based linear-cavity modeled loosely on [4] (see Fig. 1). Each end facet of the fiber cavity is connectorized with a pc connector. One end of the laser cavity is formed by sandwiching a SAM between the pc connector at the fiber end and a second pc connector, which is known as the butt-coupled technique. The output coupler at the other end of the laser cavity is similarly formed by another pc connector, which is butt-coupled with a cover glass plate coated with 35 nanometers of gold. The gold coated facet is directly connected to the pc connector of the cavity end. It is sufficient to monitor the repetition rate of only a single laser for the self-calibrating data analysis technique in the ranging applications. Therefore, we designed two output ports. One output port is the gold reflector (Out 1), and the other is the Wavelength Division Multiplexing (WDM) port of the Polarizing Beam splitter (PBS) rejection channel (Out 2). An intra-cavity polarizer simultaneously provides the polarization selectivity and an input channel for the 1480 nm pump light. The gain is provided by a 31 cm section of highly doped (80 dB/m) Er fiber with 8 µm core diameter. One of the lasers employed a tunable optical delay for the cavity length adjustment, and resulted in the repetition rate difference tunable from 0 Hz to 500 kHz for the asynchronous sampling.

Fig. 1. Design for the fiber laser. SMF- single mode fiber, PMF- polarization maintaining fiber, SAM- saturable absorber mirror

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Abstract: Two types of the dual mode-locked fiber lasers for asynchronous absolute distance measurement are investigated. The lasers are linear and ring cavity with repetition rate of 70 MHz and 100 MHz, respectively. The group velocity dispersion is not compensated in the first type of the lasers, while the others are fully done. The timing jitter with the Allan deviation below averaging time of 0.2 s during the distance measurement for around 1 m. We concluded that the phase noise resulted from the intra-cavity dispersion is the main contribution of both types of lasers were 2.5 ps with 600 nm and 1.6 ps with 200 nm. We concluded that the phase noise resulted from the intra-cavity dispersion is the main contribution for the uncertainty of the ranging in these two types of the lasers.
The difference in repetition rate of both lasers is tuned to ~1 kHz, providing an experimental update rate of only ~1 ms. Repetition rates of both lasers are not stabilized by any controller and just roughly measured by frequency counters. The lasers were housed in a box as shown in Fig. 2 with dimension of 32 cm × 28 cm × 9.5 cm to protect them from air currents and robust handling, but no temperature control or active feedback was used to otherwise stabilize their output.

The laser is started lasing with pumping laser diode (LD) current ~100 mA. As the pumping current tuned up to 200 mA, the fiber laser is started mode-locking. After fine tuning the polarization controller, the output power is increased up to 12 mW as the pumping current increased to 370 mA. The stable radio frequency (RF) spectrum with a fundamental frequency of ~70 MHz of the laser is acquired from the detector that impinged by the output of gold reflector. It can be employed as the monitor port of the laser repetition rate via RF frequency counter by further filtering and amplifier during the absolute distance measurement applications.

A2. Ring cavity mode-locked laser with full dispersion compensation

The dual laser cavities are designed as similar as our previous laser [5]. The dispersion is well controlled to around zero with compare to the previous design of positive GVD. A SAM for sustaining the mode-locking easier was also utilized in this cavity. The output power of dual lasers are >10 mW with pulse width < 100 fs.

B. Absolute distance measurement

The absolute distance measurement is realized by using these dual ultrafast fiber lasers in a time-domain down-sampling configuration [1] as shown in Fig. 3. The probe laser is retro-reflected off a pc connector and a movable corner cube to form the measurement path. The overlap between the two reflected probe pulses and local oscillator (LO) pulses is digitized synchronously with the LO comb pulses and stored for analysis. The output signal was connected to a low pass filter (LPF) to meet the Nyquist sampling condition [1]. The beating signal to noise ratio is ~ 20 dB, and is ready for the data acquisition.

The analyzing procedure is shown in Fig. 4. The raw data is Hilbert transformed to generate the imaginary component of the complex analytic representation of the signal from the real part. The carrier oscillations can then be removed by taking the modulus of this complex analytical signal to leave only the modulus, or signal envelope. The different pulses are then fit with a series of Gaussians to find the peak centers across the interferogram. For these well-behaved spectra, a Gaussian fit was well matched to the observed shape. We identify a target and reference reflection and, for each interferogram, calculate the time delay between the target and reference pulse (pk11) and the time delay between subsequent reference pulses (pk12) both in units of the pulse sample number. The distance is calculated as shown in the flow chart.

### III. Results and discussions

A. Results of ranging uncertainty and timing jitter

The ranging and timing jitter of both types of lasers are described.
A1. Ranging uncertainty and timing jitter of the non-dispersion compensated linear cavity laser

The envelope of peaks for measuring the absolute distance is ~1 m. The Allan deviation is calculated from the data as shown in Fig. 5. The measurement precision is 20 μm at the minimum acquisition time of 0.8 ms (set by the 1.25 kHz difference in laser repetition rates), and dropping ~600 nm at 200 ms averaging periods. The result is not as good as our previous ranging data by higher repetition rate with shorter fiber length design [2]. It might because of the much more positive dispersion induced phase noise in the longer fiber length of 70 MHz laser. The uncertainty of the distance measurement by pulse time of flight method is mainly from the timing jitter. The timing jitter, which calculated from the phase noise, is attributed by many reasons [6]. The relative crucial parameter is the cavity GVD.

We employed a commercial phase noise measurement machine (PN9000) for checking the timing jitter of the laser. The phase noise with respect to the frequency is shown in Fig. 6. The signal is acquired from the repetition rate signal of the linear cavity with mode-locked fiber laser. The integrated PSD (i.e. timing jitter) from 1 Hz to 1 MHz is about 2.5 ps.

A2. Ranging uncertainty and timing jitter of the well dispersion compensated fiber laser

We compare the ranging uncertainty with the ring cavity type, dual zero dispersion 100 MHz free running mode-locked lasers. The calculated Allan deviation from the ranging of ~1 m data is shown in Fig. 6. The measurement precision is 6 μm at the minimum acquisition time of 0.4 ms (set by the 2.5 kHz difference in laser repetition rates), and dropping 200 nm at 200 ms averaging periods. It is better than our non-dispersion compensated laser performed distance measurement.

The repetition rate of the ring cavity with zero GVD mode-locked fiber laser was acquired from a photodetector. It is connected to a commercial phase noise measurement machine for checking the timing jitter of the laser. The phase noise with respect to the frequency is shown in Fig. 7. The signal is acquired from the repetition rate signal of the ring cavity with well dispersion compensated mode-locked fiber laser. The integrated PSD (i.e. timing jitter) from 1 Hz to 1 MHz is about 1.5 ps.

B. Comparison and discussions

The timing jitters of these two types of the mode-locked lasers are 2.5 ps and 1.5 ps, respectively. The larger timing jitter in the 70 MHz laser is mostly attributed to the larger phase noise during the frequency of 10 Hz to 100 Hz. It is also possible
resulted from the environmental low frequency vibration noise. However, it is acquired in the same laboratory and nearly at the same time, therefore, it should be mostly resulted from the GVD induced noise. Both types of lasers are not temperature controlled in the base plate of the fiber. Although the timing jitter between these types of the lasers is only about 1.6 times, the uncertainty of the time of flight ranging is about 3 times. It could be explained that the asynchronous sampling requires dual laser for the ranging, the timing jitter induced time of flight uncertainty will thus be doubled. Although our previously 200 MHz laser performed better results [2], the cavity length is shorter than our new 70 MHz laser, and performed much smaller dispersion and uncertainty during the ranging.

IV. Conclusions
We had established dual compact and repetition rate difference tunable free running mode-locked fiber laser based ranging system. The pulse time-of-flight yields a measurement precision of 600 nm with non-ambiguity range of 2.1 m in 200 ms for distance of ~1 m. The calculated Allan deviation below averaging time of 0.2 s during the distance measurement of ~ 1 m with the timing jitter compared to 100 MHz ring cavity with zero GVD mode-locked fiber lasers were 600 nm with 2.5 ps and 200 nm with 1.6 ps, respectively. We concluded that the uncertainty of the ranging is attributed to the intra-cavity dispersion induced phase noise.

References